# Singularity, dynamics, and kinetics analysis of a 5 degrees of freedom parallel robot using screw theory 

S. Khosravi ${ }^{1,2}$, M. Ghassabzadeh Saryazdi ${ }^{\text {** }}$<br>${ }^{1}$ Technology Institute of Mechanical Engineering, Amirkabir University of Technology, Tehran, Iran<br>${ }^{2}$ Mechanical Engineering Department, Amirkabir University of Technology, Tehran, Iran


#### Abstract

This paper examines a parallel robot with 5 degrees of freedom with a linear platform. Parallel robots have a restricted workspace, and singularities make the workspace even more confined. So the behavior of the robot in the workplace is examined by focusing on kinematics and dynamics. To do kinematic analysis, the constraint equations are developed using the geometric relations, and the speed and acceleration equations of the robot are derived. The Jacobian matrix is then calculated using the screw theory, and the state of the singularities in the workspace is determined based on the Jacobian matrix. Considering the singularity and physical and geometric limitations, an algorithm for calculating the workspace is presented. In addition, the kinematic index of dexterity is investigated using the Jacobian matrix as a measure of the robot's closeness to the singular configurations. The results of solving kinematic and dynamic problems are validated with the output of the simulation in MATLAB software.


## Review History:

Received: Feb. 20, 2023
Revised: May, 13, 2023
Accepted: Oct. 03, 2023
Available Online: Nov. 04, 2023

[^0]
## 1- Introduction

During recent decades, the machine tool industry has discovered the potential benefits of parallel mechanisms and many parallel mechanisms with 5 and 6 degrees of freedom structures have been developed [1]. Parallel robots have significant advantages in machining applications, especially the machining of complex surfaces, due to the ratio of their weight to the load capacity they bear, as well as their suitable orientations in space.

The current research robot is a 5 -degrees-of-freedom parallel robot with 4SPRR-SPR configuration. In [2] Garrett et al analyzed the inverse kinematics of this structure. In [3], considering a robot with this structure, Boras et al. investigated the changes in the connection point of the robot's legs to the ground from the point of view of singularities. In [4], in addition to kinematic analysis, Guo et al analyzed the stiffness of this structure by applying the screw theory. Reference [5] is in the limited category of research that has dealt with the dynamic analysis of this structure, in which the dynamics of the robot has been extracted by the method of Kane's equations.

Screw theory, inspired by Newton-Euler relations, analyzes the dynamics of multibody systems in a matrix form, in addition to having the advantages of Lagrange equation and Newton-Euler method and high calculation speed, it
*Corresponding author's email: mghsaryazdi@aut.ac.ir
is efficient for multibody systems with a high number of members.

In this article, the inverse kinematics calculations of the robot are first performed, then the Jacobian matrix is extracted using the screw theory. All singular orientations of the robot are obtained at every point of the working space. The kinematic index of dexterity is presented as a measure of the proximity of the robot to its singular points in the workspace. The dynamics of the robot are analyzed using the screw theory. Finally, all the obtained results are validated by simulating in MATLAB's sim-mechanics environment.

## 2- Modeling

The five-degree-of-freedom robot of the current research has a 4SPRR-SPR structure, Figure 1 shows how to connect the legs of the robot to the end effector and the fixed base.

The screw axes of the robot joints are shown in Figure 3. In equation (1), the Jacobian matrix of the robot is written, which is obtained based on the screw theory

$$
J=\left[\begin{array}{cc}
O N_{1} \times S_{1,4} & S_{1,4}  \tag{1}\\
O N_{2} \times S_{2,4} & S_{2,4} \\
O N_{3} \times S_{3,4} & S_{3,4} \\
O N_{4} \times S_{4,4} & S_{4,4} \\
O N_{5} \times S_{5,4} & S_{5,4} \\
O M_{1} \times S_{1,1} & S_{1,1}
\end{array}\right]
$$

Copyrights for this article are retained by the author(s) with publishing rights granted to Amirkabir University Press. The content of this article is subject to the terms and conditions of the Creative Commons Attribution 4.0 International (CC-BY-NC 4.0) License. For more information,


Fig. 1. 5 degrees of freedom parallel robot configuration


Fig. 3. Joint screw in the robot

In screw theory, the dynamic relationships of each member are written separately, and by assembling all the equations, matrix relationships are obtained to extract the forces of operators and reaction forces.

$$
t_{i}=\left[\omega_{i}^{T} V_{i}^{T}\right]^{T}, t=\left[\begin{array}{lll}
t_{1}^{T} & t_{2}^{T} \ldots t_{n-1}^{T} \tag{2}
\end{array}\right]^{T}
$$

$$
\left[\begin{array}{cc}
K^{T} & T^{A c}  \tag{3}\\
S^{T} & o
\end{array}\right]\left[\begin{array}{l}
\lambda \\
\tau
\end{array}\right]=\left[\begin{array}{c}
\eta \\
0
\end{array}\right]
$$

$$
\begin{equation*}
\eta=M \dot{t}+W M t-w^{s} \tag{4}
\end{equation*}
$$

where the matrix $K$ with dimensions $6 n \times 6(n-1)$ contains the constraint coefficients of all kinematic pairs, which is called the robot constraint matrix. t is a $6(n-1)$ vector that includes the twist of all links of the robot. is the wrench vector of constraint torques and forces, also $T^{A c}$ called the actuator wrench shaping matrix. M is the mass matrix of the robot and W is the angular velocity matrix o-f the robot, is the vector of external forces acting on the robot.


Fig. 2. Schematic of the end effector


Fig. 4. The driving force the actuators and the error percentage with the simulation results

## 3- Results and discussion

The results of the analytical model based on the screw theory and sim-mechanics simulation are presented in Figure 4.

The physical interpretation of orientations in which the determinant of the Jacobian matrix becomes zero and the robot is placed in a singular state is shown in Figure 5.

The working space of the robot is obtained for any orientation, taking into account the constraints of equation (10). the workspace for a specific orientation is illustrated in Figure 6.

$$
\begin{equation*}
\left.|J| \neq 0, L_{i_{\min }} \leq L_{i} \leq L_{i_{\text {max }}}, 5^{\circ} \leq \pi-\beta_{i}\right) \leq 85^{\circ} \tag{5}
\end{equation*}
$$

The kinematic dexterity index is defined as a measure of how close the robot is to its singular configurations.

$$
\begin{equation*}
D I=\frac{\sigma_{\min }}{\sigma_{\max }} \tag{6}
\end{equation*}
$$

where $\sigma_{\text {min }}$ is the smallest singular value of the Jacobian matrix and $\sigma_{\max }$ is its largest singular value. Figure 7 shows


Fig. 5. Robot orientation in a singular configuration


Fig. 6. Workspace for $\alpha=0, \gamma=\pi / 6$


Fig. 7. Dexterity index distribution in a square space at a height of $\mathbf{z}=\mathbf{0 . 2 5 m}, \alpha=51^{\circ}$
the contour of the robot's dexterity for an optimal position and orientation.

## 4- conclusion

The aim of this research is the kinematic and dynamic analysis of a parallel robot. The Jacobian matrix and the dynamic equations of the robot were derived using the screw theory. By calculating the Jacobian matrix, singular points of the robot were extracted and by applying physical constraints, an algorithm was presented to calculate the working space of the robot. Then, the dexterity index was presented as a measure of the distance of the robot from singular points. This index was checked in the working space of the robot and it was determined that the robot has the highest value of dexterity index at the height of $\mathrm{z}=0.25 \mathrm{~m}$ and $\alpha=51^{\circ}$.

## References

[1] F. Gao, B. Peng, H. Zhao, W. Li, A novel 5-DOF fully parallel kinematic machine tool, The International

Journal of Advanced Manufacturing Technology, 31(1) (2006) 201-207.
[2] G.F. Bär, G. Weiß, Kinematic analysis of a pentapod robot, Journal for Geometry and Graphics, 10(2) (2006) 173-182.
[3] J. Borràs, F. Thomas, Singularity-invariant leg substitutions in pentapods, in: 2010 IEEE/RSJ International Conference on Intelligent Robots and Systems, IEEE, 2010, pp. 2766-2771.
[4] Q. Guo, G. Cui, F. Zhang, J. Liu, Z. Cheng, Kinematics. Stiffness and Singularity Analysis of 3T2R 5-DOF Parallel Robot Mechanism, in: 2019 IEEE 9th Annual International Conference on CYBER Technology in Automation, Control, and Intelligent Systems (CYBER), IEEE, 2019, pp. 758-763.
[5] W. Lin, B. Li, X. Yang, D. Zhang, Modelling and control of inverse dynamics for a 5-DOF parallel kinematic polishing machine, International Journal of Advanced Robotic Systems, 10(8) (2013) 314.

## HOW TO CITE THIS ARTICLE

S. Khosravi, M. Ghassabzadeh Saryazdi, Singularity, dynamics, and kinetics analysis of a 5 degrees of freedom parallel robot using screw theory, Amirkabir J. Mech Eng., 55(8) (2023) 197-200.



[^0]:    Keywords:
    Kinematics and dynamics
    singularity analysis
    workspace analysis
    screw theory
    parallel robot

